



## Full Length Article

# Directly catalytic reduction of NO without NH<sub>3</sub> by single atom iron catalyst: A DFT calculation

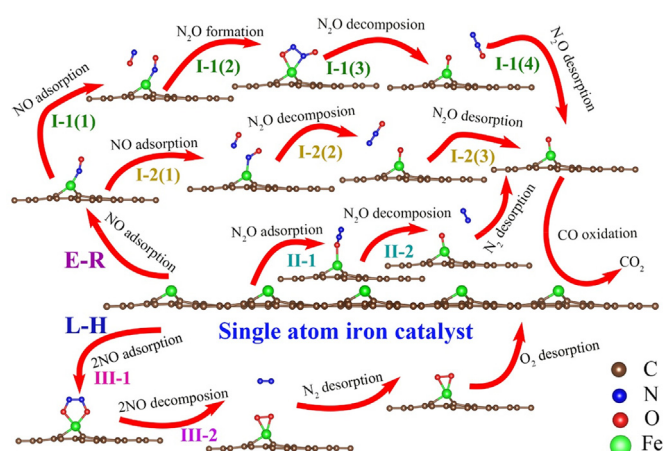


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## GRAPHICAL ABSTRACT



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## ABSTRACT

Nitric oxide (NO) has been recognized as a major air pollutant, and the emission of NO has been strictly regulated. The technology of selective catalytic reduction of NO with NH<sub>3</sub> injection is mature and efficient, but it still has some obvious drawbacks such as ammonia slipping, secondary fine particulates formation, and equipment corrosion. Therefore, a directly catalytic reduction of NO without ammonia injection by mono-vacancy graphene-based single atom iron catalyst (Fe/MG) was proposed. The detailed reaction mechanism was investigated through density functional theory calculation. Based on thermodynamic and kinetic analysis, we concluded that Langmuir-Hinshelwood is the dominant reaction mechanism for NO reduction, and the activation energy is 0.81 eV which is lower than char edges. The catalytic reduction reaction of NO is exothermic and thermodynamically favorable. The temperature can accelerate the catalytic reduction of NO. Based on the thermodynamic and kinetic performances of Fe/MG in NO reduction, Fe/MG is suggested to be a novel catalyst for NO reduction without NH<sub>3</sub>. This theoretical research results can provide a new insight for NO removal and lay some foundations for subsequent experimental research.

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## 1. Introduction

Nitrogen oxide (NO<sub>x</sub>) contains nitric oxide (NO), nitrogen dioxide (NO<sub>2</sub>), and nitrous oxide (N<sub>2</sub>O), which can lead to various environmental pollutions such as acid rain, photo-chemical smog and ozone depletion. NO<sub>x</sub> released from coal-fired power plant has been considered as the main anthropogenic source, hence, the emission standard of NO<sub>x</sub> is strictly regulated to be 50 mg/Nm<sup>3</sup> [1]. NO is the main component of NO<sub>x</sub>, making it imperative to remove NO from fuel gas.

Currently, the selective catalytic reduction with ammonia injection (SCR-NH<sub>3</sub>) has been recognized as the most mature and efficient technology for emission reduction of NO<sub>x</sub> in coal-fired power plant. However, there are still some problems for the technology of SCR-NH<sub>3</sub> in the operation process, such as ammonia slipping [2], secondary fine particulates formation [3], and equipment corrosion [4]. Moreover, the traditional catalysts for SCR-NH<sub>3</sub> (V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> and WO<sub>3</sub>/TiO<sub>2</sub>) are toxic, and will become hazardous waste after 2–3 years operation [5]. Therefore, developing a green catalyst which can directly reduce NO without ammonia injection is conducive to solve the above problems.

Single atom catalysts (SACs) are novel catalysts that can build a bridge between homogeneous catalysis and heterogeneous catalysis [6,7]. Due to its high catalytic activity, selectivity, and utilization, SACs have become the research hotspots in energy [8,9], environmental protection [10–12], and chemical engineering [13,14]. SACs have been demonstrated to have super catalytic activity in CO oxidation [15], CO<sub>2</sub> reduction [10,11], CH<sub>4</sub> activation [16] and oxygen reduction reaction [17,18]. Graphene has large specific surface area with unique physical and chemical properties, making it to be an excellent two-dimensional catalyst support. Embedding transition metal atoms into the surface of graphene-based support (TM/GS) to synthesize SACs can lower cost and improve catalytic activity [19]. Given its high catalytic activity and environment-friendly, TM/GS seems to be a potential candidate for NO reduction.

Moreover, there were some theoretical researches on the adsorption and catalytic reduction of NO under the similar system of TM/GS, which can further support and rationalize the above suppose. The adsorption of NO on the surface of metal phthalocyanines (M-PC, M = Mn, Fe, Co) was studied through density functional theory (DFT) calculation, and the adsorption energies of NO on Mn-PC, Fe-PC and Co-PC were −1.74 eV, −1.90 eV, and −1.55 eV, respectively [20]. The adsorption energies of NO and (NO)<sub>2</sub> on the surface of iron porphyrin were −2.00 eV and −2.54 eV, respectively, and the strong interaction between Fe and N may promote the reduction reaction of NO [21]. In addition, NO can be reduced into N<sub>2</sub>O on the surface of iron porphyrin, and the energy barrier in the dimer form is 0.92 eV [21]. The energy barrier of N<sub>2</sub>O dissociation to N<sub>2</sub> on the surface of Ti/GS is 2.34 eV [22], and the energy barrier of N<sub>2</sub>O decomposition on carbon-doped boron nitride nanosheet is 2.19 eV [23]. The NO can be reduced into N<sub>2</sub> by CO on the surface of Ti-porphyrin, and the rate-determining step is the desorption process of CO<sub>2</sub> [24].

Based on the above researches, it is reasonable to assume that the catalytic reduction of NO can occur on TM/GS, and TM/GS may be a promising candidate for the catalytic reduction of NO. However, the previous researches were relatively scattered and lacked systematic investigation. Therefore, a systematic research of NO reduction on TM/GS is urgently needed to explore the feasibility of practical application at the molecular level. According to the previous studies, monovacancy graphene-based single atom iron catalyst (Fe/MG) has high catalytic activity for CO oxidation [25,26] and NO oxidation [27]. In addition, Fe/MG has high adsorptivity for many toxic gases, such as NO, CO, HCN, and SO<sub>2</sub> [28,29]. Therefore, it is reasonable to expect that Fe/MG has high catalytic activity on NO reduction, and Fe/MG was selected as the research catalyst.

To explore feasibility and reaction mechanism at molecule level, we investigated the directly catalytic reduction of NO without NH<sub>3</sub> on Fe/MG. Firstly, the adsorption characteristic of NO on Fe/MG was

investigated to lay a foundation for the reaction path analysis. Secondly, the reaction paths of NO reduction on Fe/MG were systematically studied based on Langmuir-Hinshelwood (L-H) and Eley-Rideal (E-R) reaction mechanism. Additionally, thermodynamic analysis was carried out to study the effect of temperature on thermodynamic equilibrium. Moreover, the detailed kinetic analysis of two reaction mechanisms were discussed to determine the dominant mechanism. This systematic theoretical research can provide a new insight for the removal of NO and lay some foundations for subsequent experimental research.

## 2. Calculation method

The Perdew-Burke-Ernzerhof (PBE) functional and projector augmented wave (PAW) potentials were adopted to complete the DFT calculations [30–32], which has been proved to be a suitable method in the system of TM/GS [33,34]. In detail, the spin polarization correction was included in the calculation to consider the magnetism of Fe atom [28]. Consistent with our previous study [29], a 4 × 4 graphene with vacuum layer of 15 Å was used to simulate the surface of Fe/MG. The calculation software was Vienna ab initio simulation package (VASP 5.4.1).

To obtain accurate calculation results with less computational cost, a 7 × 7 × 1 Γ-centered k-point and 500 eV cutoff energy were adopted in the calculation of geometric optimization based on our previous test [35,36]. With regards to geometry optimization, all atoms were allowed to fully relax with force convergence standard of 0.02 eV/Å and energy convergence standard of 10<sup>−5</sup> eV. Based on the optimized geometry, a denser k-point (15 × 15 × 1) was adopted in the calculation of self-consistent field to obtain more accurate system energy, density of states (DOS), and Bader charge [37].

To locate the transition states rapidly and accurately, two methods of climbing-image nudged elastic band (CI-NEB) [38,39] and improved dimer method (IDM) [40] were applied together. Approximate structures of transition state was rapidly determined by CI-NEB method with a 0.1 eV/Å force convergence. Based on the possible transition state structures calculated by CI-NEB, the final transition state structures was accurately located by IDM with the force convergence of 0.05 eV/Å. Additionally, vibrational frequency with finite displacements of ± 0.02 Å [41,42] was calculated to validate the transition state structures and obtain the zero point energy correction.

The adsorption energy ( $E_{ads}$ ) can be calculated according to Eq. (1).

$$E_{ads} = E_{tot} - E_{gas} - E_{sur} \quad (1)$$

where  $E_{tot}$ ,  $E_{gas}$  and  $E_{sur}$  are the ground-state energy of adsorption systems, adsorbates, and Fe/MG, respectively.

To describe the difficulty degree of reaction process, the energy barrier ( $E_b$ ) was calculated according to from Eq. (2).

$$E_b = E_{TS} - E_{IS} \quad (2)$$

where  $E_{TS}$  and  $E_{IS}$  are the system energy of transition and initial state, respectively.

Thermodynamic properties of reduction reaction was discussed through analyzing the equilibrium constant which can be calculated from the following Eq. (3) [43]:

$$\Delta G = G_{FS} - G_{IS} = -RT \cdot \ln K \quad (3)$$

where  $G_{FS}$  and  $G_{IS}$  are Gibbs free energy of final and initial state;  $R$  is the universal gas constant;  $T$  is the temperature;  $K$  is the equilibrium constant.

The Gibbs free energy of solid surface and gases was calculated from the Eqs. (4) and (5) [36]:

$$G_{solid}(T) = E_{ele} + ZPE - TS \quad (4)$$

$$G_{gas}(T) = E_{ele} + ZPE + RT - TS \quad (5)$$

where  $E_{ele}$  is the system energy in ground state obtained from self-

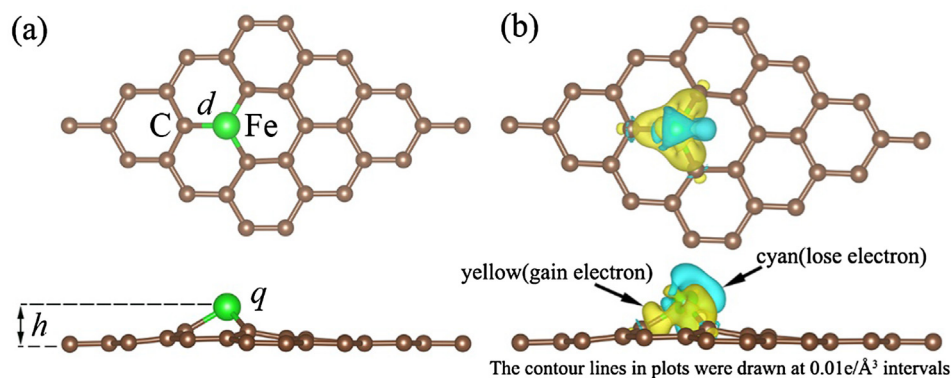


Fig. 1. The geometric structure and electron density difference of Fe/MG.

consistent field calculation; ZPE is the zero point correction energy calculated from vibrational frequency calculation;  $S$  is entropy (The entropies of adsorbed systems and gases are obtained from vibrational frequency calculation [44] and NIST database [45], respectively);

According to the transition state theory, the reaction rate constant was calculated to study the kinetic properties of reduction reaction, and the calculation formula was shown in Eq. (6) [43]:

$$k^{TST} = \frac{k_B T}{h} \times \left( \frac{RT}{P_0} \right)^{\Delta n} \times \exp\left( \frac{-\Delta G_b}{k_B T} \right) \quad (6)$$

where  $h$  is the Planck constant;  $k_B$  is the Boltzmann constant;  $\Delta n = 0$  (unimolecular reaction) or 1 (bimolecular reaction);  $P_0$  is the standard atmospheric pressure;  $\Delta G_b$  is the energy barrier in Gibbs free energy.

### 3. Results and discussion

#### 3.1. The research model

The optimized structure and electron density difference of Fe/MG were plotted in Fig. 1, the detailed calculation process of electron density difference can be seen in Fig. S1. The corresponding structural and electronic parameters were summarized in Table 1. From Fig. 1(b), the Fe atom was surrounded by the cyan color and the adjacent C atoms were surrounded by the yellow color, which indicates that the electron transfers from Fe atom to graphene-based supports in the doping process of Fe atom. In addition, the charge of Fe atom was 0.69 e, which is consistent with the analysis of electron density difference. According to the adsorption energy of Fe atom (Table 1),  $E_{ads}$  of Fe on monovacancy graphene ( $-7.14$  eV) is obviously larger than that on perfect graphene ( $-1.04$  eV [46]) and the cohesive energy of Fe bulk ( $-4.28$  eV [47]), suggesting that Fe/MG is stable enough to avoid agglomeration and migration. Compared with the calculated results of Fe/MG and literature data, it is concluded that the research model of Fe/MG is validity and rationality.

#### 3.2. The adsorption characteristic of NO

According to the study of Wang et al [50], Fe/MG can be a promising material for CO removal in the hydrogen fuel cells. In the research of Tang et al [28], the adsorption of NO on Fe/MG belongs to strong chemical adsorption, so Fe/MG seems to be an effective

Table 1

The bond length between C and Fe ( $d$ ), the uplift height of Fe ( $h$ ), the charge of Fe ( $q$ ) and the adsorption energy of Fe ( $E_{ads}$ ) for Fe/MG.

Systems	$d$ (Å)	$h$ (Å)	$q$ (e)	$E_{ads}$ (eV)
Calculation data	1.76	1.35	0.69	$-7.14$
Literature data	1.76 [26]	1.36 [48]	0.69 [36]	$-7.15$ [49], $-7.28$ [26]

adsorbent for NO removal. To verify this assumption, the adsorption characteristic of  $(NO)_n$  ( $n = 1-4$ ) on Fe/MG was investigated. The optimized adsorption structures of  $(NO)_n$  ( $n = 1-4$ ) on Fe/MG were plotted in Fig. 2(a)–(d), and some important adsorption configurations for reaction path analysis were also plotted in Fig. 2(e)–(h). Additionally, some key parameters in adsorption process, such as adsorption energies, bond lengths and charge transfer, were summarized in Table 2.

Combining the Table 2 and Fig. 2(a–d), the  $E_{ads}$  increased as the number of NO increased, while the  $E_{ads/per}$  decreased as the number of NO increased. Meanwhile, the average bond length between N and Fe ( $d_{N-Fe}$ ) increased as the number of NO increased, indicating that the adsorption strength decreases as the number of NO increases. The  $d_{N-Fe}$  obviously increased from  $1.74$  Å to  $1.94$  Å when the third NO molecule was adsorbed on Fe/MG, and the  $d_{N-Fe}$  obviously increased from  $1.94$  Å to  $2.27$  Å when the fourth NO molecule was adsorbed on Fe/MG. From the adsorption configurations of NO on Fe/MG, the maximum bond lengths between N and Fe in Fig. 2(c) and (d) were  $2.13$  Å and  $3.15$  Å, further confirming that the adsorption strength of NO on Fe/MG obviously decreases when the number of NO molecule increases to three. Different from the study of Wang et al on CO adsorption [50], Fe/MG can firmly adsorb three CO molecules at the same time, but only two NO molecules can be firmly adsorbed on Fe/MG. Therefore, Fe/MG may not be suitable as an adsorbent for NO removing, and a detailed analysis focused on the catalytic reduction mechanism was carried out in the next content.

From Table 2, it is noteworthy that there is a clear linear relationship between the amounts of charge transfer and the adsorption energies of NO on Fe/MG, except for Fig. 2(g). There was a  $-3.65$  eV adsorption energy with  $0.49$  e charge transfer for the adsorption configuration of Fig. 2(b), but there was a  $-3.35$  eV adsorption energy with  $0.91$  e for the adsorption configuration of Fig. 2(g). In order to investigate the difference between Fig. 2(b) and (g) in adsorption energy and charge transfer, the bonding characteristics of adsorption configurations in Fig. 2(b) and (g) were discussed through the projected density of states (PDOS) analysis. The PDOS of Fig. 2(b) and (g) were plotted in Figs. 3 and 4, respectively. In detail, density of states for total,  $d$  orbital of Fe atom and  $p$  orbital of two N or O atoms in NO molecules were plotted to study the interaction of Fe/MG and NO. According to the frontier molecular orbital theory, regions near Fermi energy level are critical for bonding, so some regions were circled by broken lines to investigate the hybridization between NO and Fe/MG. In the regions circled by broken lines of Fig. 3, the peaks of Fe( $d$ ) and N( $p$ ) occur at the same energy level, suggesting that there was strong hybridization between Fe( $d$ ) and N( $p$ ). However, there was no obvious strong hybridization between Fe( $d$ ) and O( $p$ ) in the regions circled by broken lines of Fig. 4. From the above analysis, it is deduced that the binding mechanism adsorption configuration of Fig. 2(g) is dominated by hybridization effect, whereas the binding mechanism adsorption

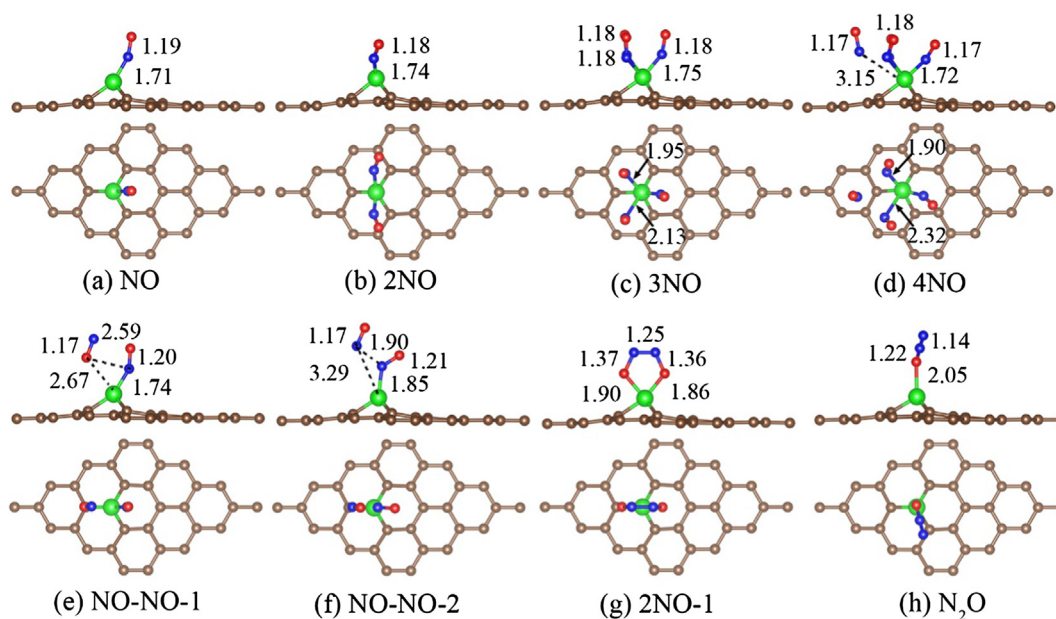


Fig. 2. The adsorption structures of NO on Fe/MG (The unit of length is Å).

Table 2

The adsorption energies of NO ( $E_{\text{ads}}$ , eV), the adsorption energy per NO ( $E_{\text{ads/per}}$ , eV), the average bond lengths between N and Fe ( $d_{\text{N-Fe}}$ , Å) and the charge variations of corresponding gases before and after adsorption ( $\Delta q$ , e). (The symbol of “+” and “-” means gain and lose electron).

Structures	$E_{\text{ads}}$ (eV)	$E_{\text{ads/per}}$ (eV)	$d_{\text{N-Fe}}$ (Å)	$\Delta q$ -gas (e)
(a) NO	-2.24 (-2.40 [28])	-2.24	1.71	+0.34 (+0.43 [28])
(b) 2NO	-3.65	-1.82	1.74	+0.49
(c) 3NO	-3.98	-1.33	1.94	+0.55
(d) 4NO	-4.61	-1.15	2.27	+0.63
(e) NO-NO-1	-2.64	-1.32	2.21	+0.41
(f) NO-NO-2	-2.56	-1.28	2.57	+0.38
(g) 2NO-1	-3.35	-1.67	-	+0.91
(h) N <sub>2</sub> O	-0.38	-0.38	-	+0.07

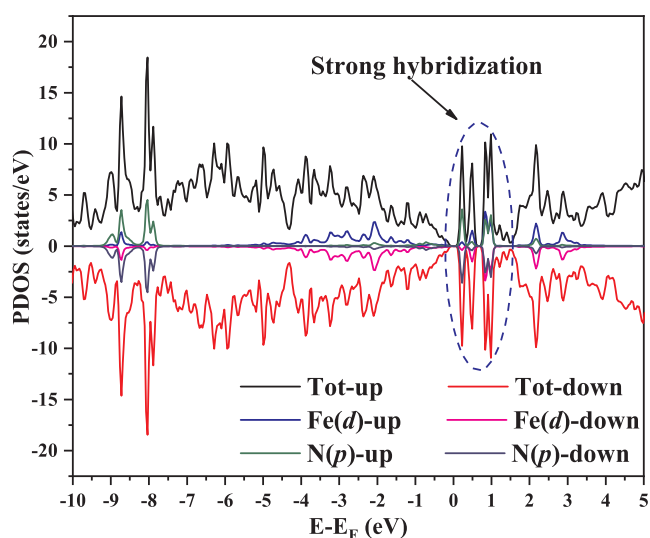


Fig. 3. The PDOS for the structure of Fig. 2(b).

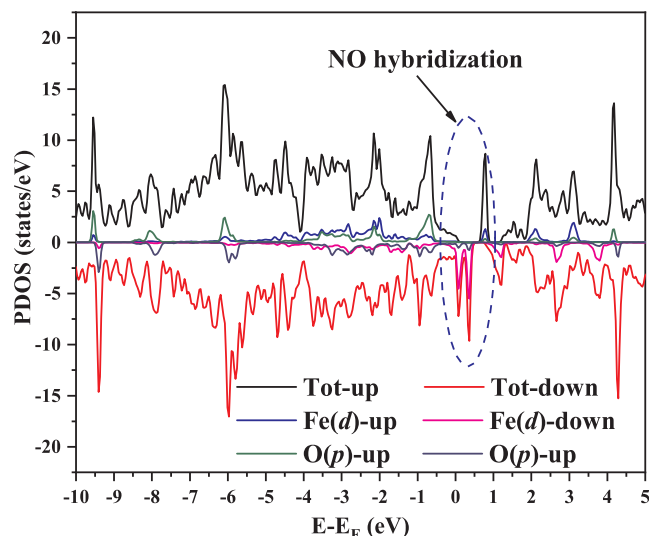


Fig. 4. The PDOS for the structure of Fig. 2(g).

configuration of Fig. 2(b) is mainly governed by charge transfer. Therefore, the difference between Fig. 2(b) and (g) in adsorption energy and charge transfer can be well understood from the view of binding mechanism.

To study the catalytic reduction of NO on Fe/MG, the possible adsorption configurations of NO and N<sub>2</sub>O on Fe/MG were calculated according to the reaction mechanism of Eley-Rideal (E-R) and Langmuir-Hinshelwood (L-H), as show in Fig. 2(e)–(h). There were two possible adsorption structures of NO on Fe/MG in Fig. 2(e) and (f). Given that there is no obvious difference between two possible adsorption configurations in adsorption energy, therefore, Fig. 2(e) and (f) were both selected as the initial reactants for E-R mechanism analysis. At the same time, the adsorption configurations of Fig. 2(b) and (g) were both selected as the initial reactants for L-H mechanism analysis.

### 3.3. Reaction path analysis

To consider the E-R and L-H reaction mechanism, we designed various reaction paths based on the adsorption configurations of two



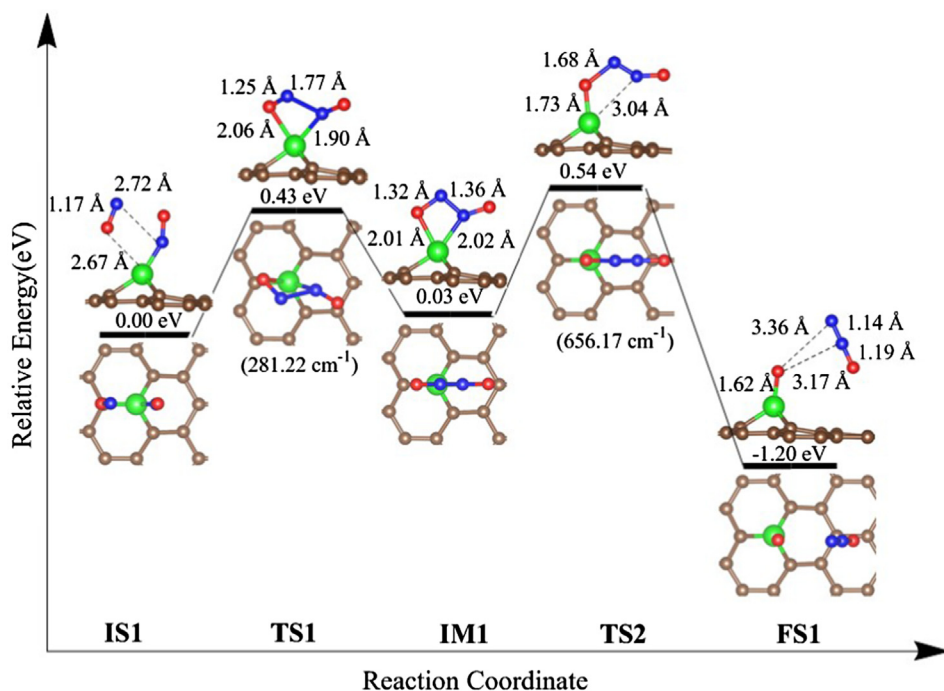


Fig. 5. The reduction reaction path diagram of NO into N<sub>2</sub>O (E-R-I-1).

NO molecules on Fe/MG (Fig. 2(b), (e)–(g)). However, no possible reaction path was found when the adsorption configuration of Fig. 2(b) was selected as initial reactant. Therefore, the reaction path in the L-H mechanism analysis which only started from Fig. 2(g), was elaborated in this work. Based on the E-R and L-H reaction mechanism, the reaction path analysis was performed respectively. Furthermore, in E-R reaction mechanism, the catalytic reduction of NO can be divided into two different reaction stages according to the reaction process. The first stage is the catalytic reduction of NO into N<sub>2</sub>O (E-R-I), and the second stage is the catalytic reduction of N<sub>2</sub>O into N<sub>2</sub> (E-R-II).

### 3.3.1. E-R reaction mechanism

**3.3.1.1. The reduction of NO into N<sub>2</sub>O.** According to the different adsorption configurations of the second NO molecule (Fig. 2(e) and (f)), there were two different reaction paths for the catalytic reduction of NO (E-R-I-1 and E-R-I-2), and the detailed reaction path diagrams were plotted in Figs. 5 and 6, respectively. In detail, the key bond length, the change of system energy (ZPE was included), and the imaginary frequency of transition state were labeled in Figs. 5 and 6.

In Fig. 5, the catalytic reduction of NO on Fe/MG started from the adsorption configuration of Fig. 2(e), and two NO molecules were reduced into N<sub>2</sub>O on Fe/MG through two transition states. Firstly, the gaseous NO molecule attacked NO which was adsorbed on Fe/MG, generating a N<sub>2</sub>O molecule with an energy barrier of 0.43 eV. Then, with the increase of Fe-N bond length (2.02 Å (IM1) → 3.04 Å (TS2) → 3.17 Å (FS1)), the formed N<sub>2</sub>O molecule desorbed from Fe/MG with an energy barrier of 0.51 eV.

In Fig. 6, the catalytic reduction of NO on Fe/MG started from the adsorption configuration of Fig. 2(f), and two NO molecules were reduced into N<sub>2</sub>O on the surface of Fe/MG through only one transition state. The NO molecule attacked the N atom of NO adsorbed on Fe/MG, and the formation and desorption of N<sub>2</sub>O were completed at the same time with the decrease of N-N bond length (1.90 Å (IS2) → 1.27 Å (TS3) → 1.14 Å (FS2)) and the increase of N-O bond length (1.21 Å (IS2) → 1.41 Å (TS3) → 3.22 Å (FS2)). Compared with the reaction path E-R-I-1 (Fig. 5), the energy barrier of catalytic reduction is 0.21 eV, which is smaller than that in E-R-I-1 (0.43 eV and 0.51 eV). Although the adsorption energy in Fig. 2(e) is relatively larger than that in

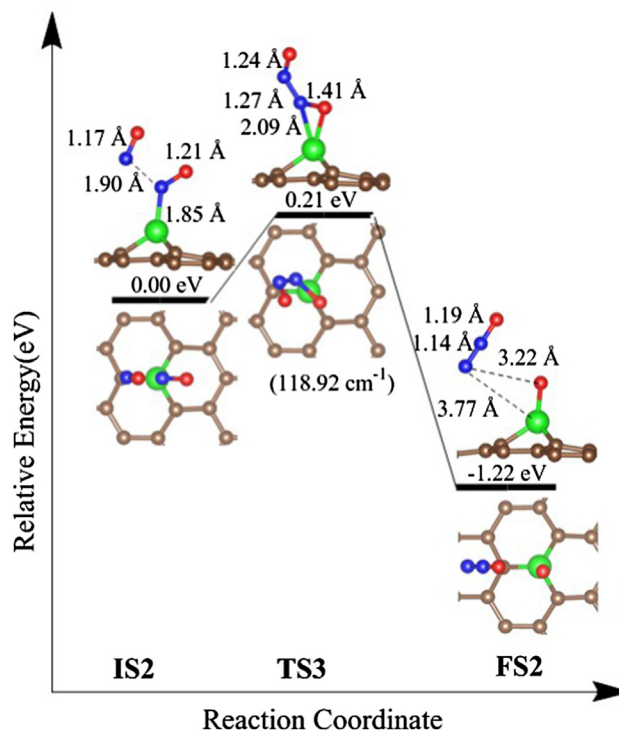


Fig. 6. The reduction reaction path diagram of NO into N<sub>2</sub>O (E-R-I-2).

Fig. 2(f), the catalytic reduction of NO in E-R-I-2 is more likely to occur than in E-R-I-1 at the view of reaction process and energy barrier.

**3.3.1.2. The reduction of N<sub>2</sub>O into N<sub>2</sub>.** Two NO molecules can be reduced into N<sub>2</sub>O relatively easily on Fe/MG according to the above analysis, and the reduction of N<sub>2</sub>O into N<sub>2</sub> will be discussed in this content. The formed N<sub>2</sub>O molecule can be reduced into N<sub>2</sub> on Fe/MG, the detailed reaction path was plotted in Fig. 7. From Fig. 7, with the increase of N-O bond length (1.22 Å (IS3) → 1.39 Å (TS4) → 3.07 Å

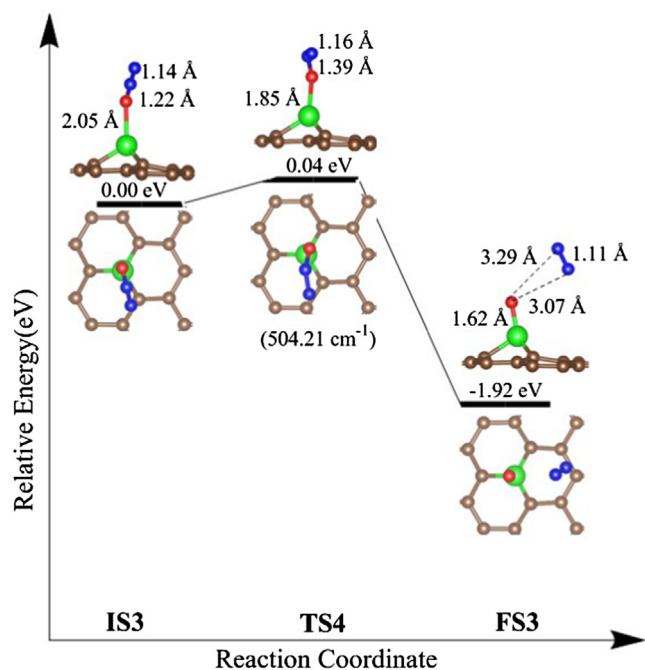


Fig. 7. The reduction reaction path diagram of  $N_2O$  into  $N_2$  (E-R-II).

(FS3), the  $N_2O$  molecule was decomposed into  $N_2$  under the catalytic effect of Fe/MG. The decomposition of  $N_2O$  into  $N_2$  can easily take place with a 0.04 eV energy barrier, and the decomposition of  $N_2O$  is an exothermic process (1.92 eV). The decomposition of  $N_2O$  is barrierless and thermodynamically favorable, so the decomposition of  $N_2O$  can take place at the room temperature. Compared with the reduction of  $N_2O$  into  $N_2$  on the surface of Co/SV [51], the energy barrier of on Fe/MG (0.04 eV) is lower than that on Co/SV (0.1 eV), indicating that Fe/MG has higher catalytic activity than Co/SV.

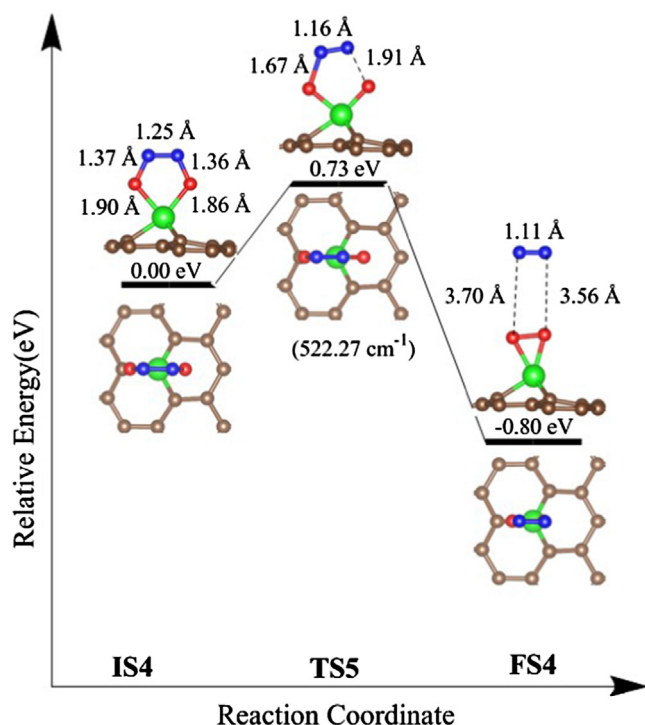


Fig. 8. The reaction path diagram of NO reduction (L-H).

### 3.3.2. L-H mechanism

In L-H mechanism, the catalytic reduction of NO started from Fig. 2(g), and the detailed reaction path was plotted in Fig. 8. From Fig. 8, two adsorbed NO molecules was activated under the activation effect of Fe/MG, the N-O bond lengths of two adsorbed NO molecules (1.36 Å and 1.37 Å) are all larger than the bond length of gaseous NO molecule (1.15 Å) [52]. With the increase of N-O bond length (1.37 Å (IS4) → 1.67 Å (TS5) → 3.70 Å (FS4) and 1.36 Å (IS4) → 1.91 Å (TS5) → 3.56 Å (FS4)), the  $N_2$  molecule desorbed from Fe/MG through a medium energy barrier (0.73 eV). Similar to E-R mechanism, the reduction reaction was also exothermic progress (0.80 eV) in L-H mechanism.

For recover of catalyst, the desorption process of residual oxygen atom and  $O_2$  adsorbed on the surface of Fe/MG should be investigated. Many studies have shown that the residual oxygen atom and  $O_2$  adsorbed on the surface of Fe/MG can react with CO to produce  $CO_2$  with a low energy barrier [25,26]. There are about 500 ppm CO in the flue gases, and the residual oxygen atom should be easily consumed by CO. Given that the main purpose of this study is to reveal the mechanism of NO catalytic reduction, so the detailed reaction paths between residual oxygen (O atom and  $O_2$ ) and CO will not be discussed in this work.

Comparing E-R mechanism and L-H mechanism, the catalytic reduction of NO in E-R and L-H mechanism were both exothermic process and thermodynamically favorable. The catalytic reduction of NO in L-H mechanism occurred through only one transition state, but there were two stages for catalytic reduction of NO in E-R mechanism. However, the energy barrier in E-R mechanism is relatively lower than that in L-H mechanism. To further investigate the effect of temperature on the catalytic reduction of NO and confirm its dominant mechanism in E-R and L-H, the thermodynamic analysis and kinetic analysis were performed to discuss this in detail.

### 3.4. Thermodynamic analysis

To investigate the effect of temperature on the thermodynamic properties of catalytic reduction of NO and compare the difference of E-R and L-H mechanism in thermodynamic properties, the reaction Gibbs free energy ( $\Delta G$ ) and equilibrium constant (K) were calculated. Given the temperature of fuel gas, the research temperature range was selected from 298.15 K to 1000 K. The value of  $\Delta G$  were summarized in Table S1 (ESI). According to the Eq. (3), the natural logarithm of K for different reaction paths were calculated, as shown in Fig. 9.

From Table S1, except for IS1 → IM1, the reaction energies of different reaction steps under research temperature range were all negative, which indicates that the most reaction steps of NO reduction can

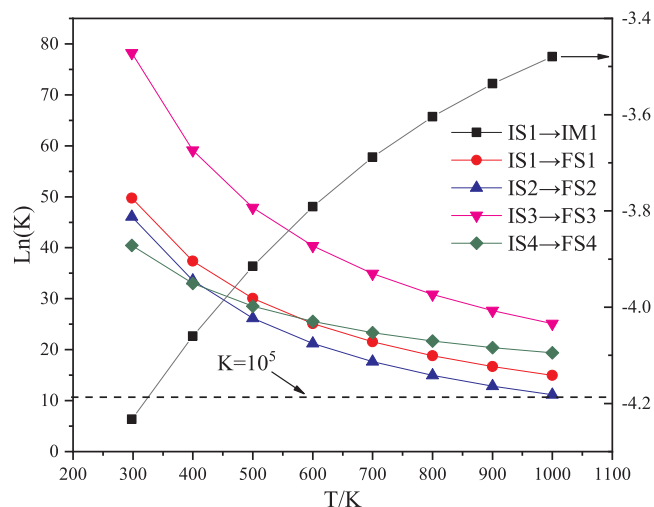


Fig. 9. The  $\ln(K)$  under different temperatures.

occur spontaneously under the research temperature range. In Fig. 9, the  $\text{Ln}(K)$  data of  $\text{IS1} \rightarrow \text{IM1}$  was plotted in right coordinate axis, and  $\text{Ln}(K)$  data of the others were plotted in left coordinate axis. From Fig. 9, the  $\text{Ln}(K)$  data of  $\text{IS1} \rightarrow \text{FS1}$  increased with the increase of temperature, whereas the  $\text{Ln}(K)$  data of the others decreased with the increase of temperature. For the reaction steps of  $\text{IM1} \rightarrow \text{FS1}$ ,  $\text{IS2} \rightarrow \text{FS2}$ ,  $\text{IS3} \rightarrow \text{FS3}$  and  $\text{IS4} \rightarrow \text{FS4}$ , the temperature has obvious inhibiting effect on reaction equilibrium, and higher temperature will promote the reaction equilibrium to the adverse direction. Although the value of  $\text{Ln}(K)$  decreased with the increase of temperature, the  $\text{Ln}(K)$  data of  $\text{IM1} \rightarrow \text{FS1}$ ,  $\text{IS2} \rightarrow \text{FS2}$ ,  $\text{IS3} \rightarrow \text{FS3}$  and  $\text{IS4} \rightarrow \text{FS4}$  under different temperatures were all larger than  $10^5$  [43], illustrating that the reaction rate of forward direction will be far greater than that of reverse direction and those reaction steps can take place completely and irreversibly. Therefore, the reaction steps of  $\text{IM1} \rightarrow \text{FS1}$ ,  $\text{IS2} \rightarrow \text{FS2}$ ,  $\text{IS3} \rightarrow \text{FS3}$  and  $\text{IS4} \rightarrow \text{FS4}$  were treated as unidirectional and forward reaction in the following kinetic analysis.

### 3.5. Kinetic analysis

To consider the effect of temperature on the kinetic characteristics of catalytic reduction of NO and compare the difference of E-R and L-H mechanism in kinetic properties, the natural logarithm of reaction rate constants ( $\text{Ln}(k^{\text{TST}})$ ) were calculated according to the Eq. (6). The  $\text{Ln}(k^{\text{TST}})$  of elementary reactions in bimolecular and unimolecular reaction were plotted in Fig. 10. The reaction rate constants of forward process were marked by positive number (such as  $k_1$ ) and the reaction rate constants of reverse process were marked by negative number (such as  $k_{-1}$ ). From Fig. 10, the reaction rate constants all increased with the increase of temperature. The  $\text{Ln}(k^{\text{TST}})$  of forward processes were all greater than zero under all of the research temperatures, whereas  $\text{Ln}(k^{\text{TST}})$  of reverse processes were mostly less than zero under most of the research temperatures. The reaction rate constants of forward processes (except for the reaction of  $\text{IS1}$  to  $\text{IM1}$ ) were all far greater than that of reverse processes, which is in accordance with thermodynamic analysis, suggesting that the catalytic reduction of NO will be mainly governed by the forward process under the research temperature range.

In order to compare the reaction rate constant of E-R and L-H conveniently, the overall reaction rate constants in E-R and L-H mechanism were further discussed in the next analysis. According to the above reaction path analysis, there was no obvious difference between two transition states in energy barrier for E-R-I-1 reaction path. Therefore, the steady state approximation theory [53], which has been proved to be reasonable for kinetics modeling, was adopted for calculating the overall reaction rate constant in E-R mechanism. In steady state

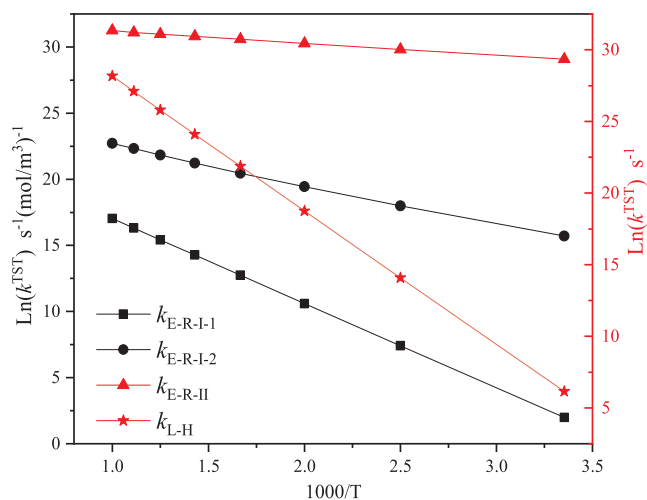


Fig. 11. The  $\text{Ln}(k^{\text{TST}})$  for different reaction steps.

approximation theory, the concentration of intermediates involved in the reaction is considered not to vary with time. The overall reaction rate constant of E-R-I-1 ( $k_{E-R-I-1}$ ) can be calculated by Eq. (7), and the detailed derivation was provided in the supporting material (ESI).

$$k_{E-R-I-1} = \frac{k_1 k_2}{k_{-1} + k_2} \quad (7)$$

In addition, the overall reaction rate constants of E-R-I-2 ( $k_{E-R-I-2}$ ), E-R-II ( $k_{E-R-II}$ ) and L-H ( $k_{L-H}$ ) are equal to  $k_3$ ,  $k_4$  and  $k_5$ , respectively. Therefore, the reaction rate constant of different reaction steps can be easily obtained based on the above reaction rate constant calculation, as shown in Fig. 11.

In Fig. 11, the bimolecular reactions and the unimolecular reactions were plotted in the black and red color, respectively. Based on above reaction rate constants, the pre-exponential factor (A) and activation energy ( $E_a$ ) were calculated. The detailed calculation steps and data were provided in Fig. S2 and Table 3, respectively. From Table 3, the activation energy of the reduction of  $\text{N}_2\text{O}$  into  $\text{N}_2$  is only 0.07 eV, which is obviously lower than that of  $\text{N}_2\text{O}$  reduction on the surface of zigzag char edges (0.34 eV) and armchair char edges (1.64 eV) [43]. Comparing the activation energy of Fe/MG and char edges, the lower activation energy of Fe/MG indicates that the Fe/MG has higher catalytic activity than the char.

Given that there were two reaction paths in the first stage of E-R mechanism, it is inconvenient to directly compare the speed of E-R and

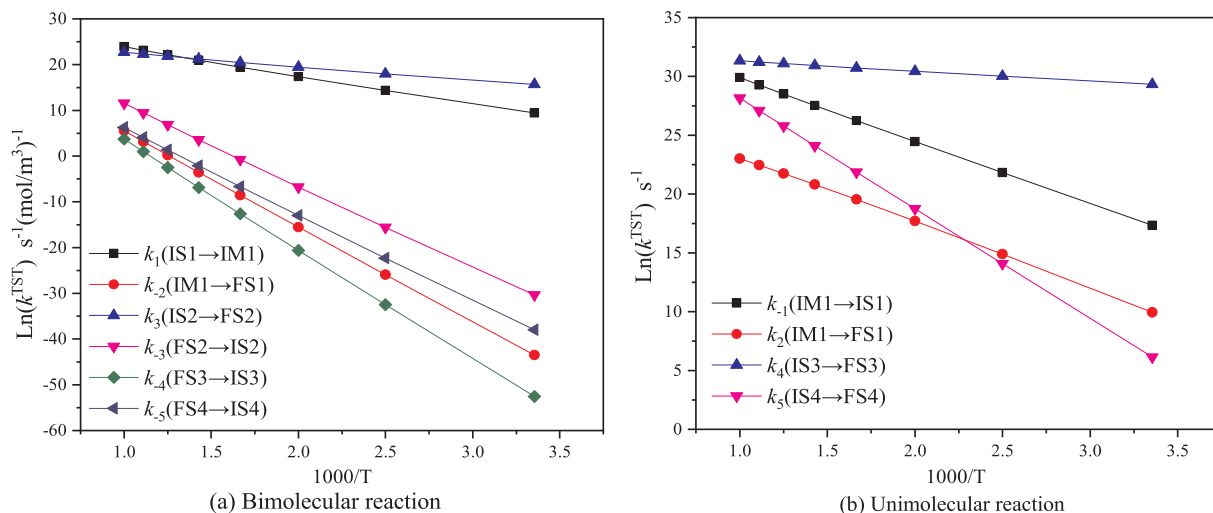
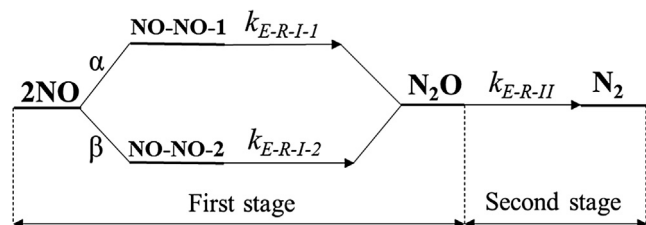


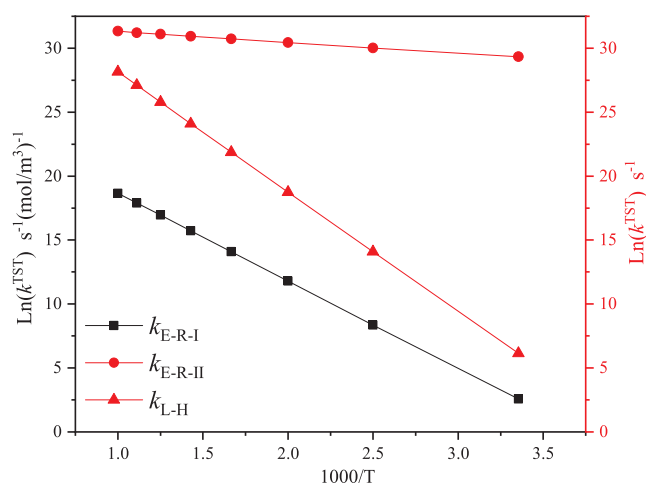
Fig. 10. The natural logarithm of reaction rate constants for different elementary reactions.

**Table 3**  
The kinetic parameters of different reaction steps.

Kinetic parameters	E-R-I-1	E-R-I-2	E-R-II	L-H
$E_a/eV$	0.55	0.25	0.07	0.81
A	$1.46 \times 10^{10} s^{-1} (mol/m^3)^{-1}$	$1.20 \times 10^{11} s^{-1} (mol/m^3)^{-1}$	$9.17 \times 10^{13} s^{-1}$	$1.87 \times 10^{16} s^{-1}$



**Fig. 12.** The schematic diagram of catalytic reaction in E-R mechanism.



**Fig. 13.** The overall reaction rate constant for different reaction mechanisms.

L-H mechanisms. Therefore, the overall reaction rate constant of first stage in E-R mechanism ( $k_{E-R-I}$ ) which includes the contribution of two pathways to the reaction rate, should be calculated. To obtain the value of  $k_{E-R-I}$ , the schematic diagram of catalytic reaction in E-R mechanism was plotted, as shown in Fig. 12.

In Fig. 12, due to different adsorption configurations (as shown in Fig. 2), there were two reaction paths in the first stage of reaction. The proportions of two adsorption configurations were  $\alpha$  and  $\beta$ , and the sum of  $\alpha$  and  $\beta$  is equal to 1 ( $\alpha + \beta = 1$ ). According to the Boltzmann distribution [50], we can get the proportional relationship between  $\alpha$  and  $\beta$  using the adsorption energy from Table 2, and the detailed calculation was shown in Eq. (8).

$$\frac{\alpha}{\beta} = \exp\left(-\frac{E_{ads}(NO-NO-1) - E_{ads}(NO-NO-2)}{k_B T}\right) \quad (8)$$

Therefore, the value of  $\alpha$  and  $\beta$  can be calculated and the detailed data was summarized in Table S2. The overall reaction rate constant of first stage in E-R mechanism ( $k_{E-R-I}$ ) was calculated from Eq. (9), and the value of  $k_{E-R-I}$  was plotted in Fig. 13.

$$k_{E-R-I} = \alpha k_{E-R-I-1} + \beta k_{E-R-I-2} \quad (9)$$

From Fig. 13, the overall reaction rate constant of second stage ( $k_{E-R-II}$ ) in E-R mechanism is obviously larger than that of first stage ( $k_{E-R-I}$ ), indicating that the reaction speed is determined by the first stage in E-R mechanism. Comparing the value of  $k_{E-R-I}$  and  $k_{L-H}$ ,  $k_{L-H}$  is larger than  $k_{E-R-I}$ , especially in high temperature. Therefore, the dominant mechanism should be L-H in the view of kinetic properties. The activation energy of NO reduction in L-H mechanism is 0.81 eV. In the catalytic reduction of

NO on char edges [54], the dominant reaction mechanism of NO reduction on the surface of char edges is E-R mechanism, and the activation energy of NO reduction on the surface of char edges is 1.08 eV. Compared with the reduction of NO on char edges, the catalytic reduction of NO on the surface of Fe/MG has lower activation energy, further confirming that Fe/MG can be a promising catalyst for NO reduction.

#### 4. Conclusion

In this theoretical research work, the mechanism of directly catalytic reduction of NO on Fe/MG was systematically studied based on the reaction path, thermodynamic and kinetic analysis. The catalytic reduction of NO in E-R mechanism can be divided into two different stages, and the rate-determining step is the first stage (the reduction of two NO molecules into N<sub>2</sub>O). The reaction of second stage (the reduction of N<sub>2</sub>O into N<sub>2</sub>) can be considered as barrierless with an activation energy of 0.07 eV. The catalytic reduction reactions of NO in L-H and E-R mechanisms are both exothermic and thermodynamically favorable. The L-H mechanism acts as the dominant role in the view of reaction kinetics, and its activation energy of NO reduction on the surface of Fe/MG is 0.81 eV. In addition, the temperature acts as a promoting effect on the catalytic reduction of NO. Based on the thermodynamic and kinetic performances of Fe/MG in NO reduction reaction, Fe/MG is suggested to be a novel catalyst for directly catalytic reduction of NO without NH<sub>3</sub>.

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#### Appendix A. Supplementary data

Supplementary data to this article can be found online at <https://doi.org/10.1016/j.fuel.2019.01.125>.

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